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## Grid geometry effects on convection in ocean climate models: a conceptual study

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### Abstract

10 Ocean convection is a highly non-linear and local process. Typically, a small-scale phenomenon of this  
11 kind entails numerical problems in the modelling of ocean circulation. One of the tasks to solve is the  
12 improvement of convection parameterization schemes, but the question of grid geometry also plays a  
13 considerable role. Here, this question is studied in the context of global ocean models coupled to an at-  
14 mosphere model. Such ocean climate models have mostly structured, coarsely resolved grids.

15 Using a simple conceptual two-layer model, we compare the discretization effects of a rectangular grid  
16 with those of a grid with hexagonal grid cells, focussing on average properties of the ocean. It turns out that  
17 systematic errors tend to be clearly smaller with the hexagonal grid. In a hysteresis experiment with the  
18 atmospheric boundary condition as a hysteresis parameter, the spatially averaged behaviour shows non-  
19 negligible artificial steps for quadratic grid cells. This bias is reduced with the hexagonal grid. The same  
20 holds for the directional sensitivity (or horizontal anisotropy) which is found for different angles of the  
21 advection velocity. The grid with hexagonal grid cells shows much more isotropic results. From the limited  
22 viewpoint of these test experiments, it seems that the hexagonal grid (i.e. icosahedral–hexagonal grids on  
23 the sphere) is recommendable for ocean climate models.

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25 *Keywords:* Oceanic convection; Ocean modelling; Parameterization; Model grid

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## 26 1. Introduction

27 To the largest part of its extent, the world ocean is stratified in a statically stable way, so that  
28 vertical exchange processes are weak. Only in a few small regions in the North Atlantic, the  
29 Mediterranean, and the Southern Ocean, a combination of wind stress forcing, freshwater ad-  
30 vection and surface heat fluxes may succeed in diminishing this stratification. In places where the  
31 vertical density gradient actually vanishes, one observes a strong vertical turbulent mixing to  
32 depths of 2 km and more. This process, occurring only for a few days at a time, and on spatial  
33 scales of only  $\sim 50$  km, is called deep convection (see Marshall and Schott (1999) for a compre-  
34 hensive review).

35 Convection constitutes a much more efficient vertical heat transfer process than vertical (dia-  
36 pycnal) mixing. Therefore it is essential for ocean general circulation models that both location  
37 and timing of convection are captured. Furthermore, convection events are a crucial part of the  
38 overturning circulation in the North Atlantic that ensures today's climatic conditions in the North  
39 Atlantic region. But the small spatial and temporal scales of convection prevent a direct repre-  
40 sentation in global ocean models that are part of a climate model (called ocean climate models  
41 here) as their resolution is too coarse. Hence, in ocean climate models, convection is parame-  
42 terized. Convective adjustment (Cox, 1984; Rahmstorf, 1993) and an increased vertical diffusion  
43 coefficient in places where the stratification is weak (Klinger et al., 1996; Molemaker and Dijkstra,  
44 2000) are the most commonly used parameterization schemes. Convection parameterizations have  
45 been studied thoroughly, but the role of the model grid geometry has been considered much less.

46 In ocean models that are not coupled to a dynamical atmosphere, unstructured grids are often  
47 used. They can be adapted to a given orography in a very efficient way. On the other hand, the  
48 coupling to an atmospheric component with its structured grid is rather complicated. This is a  
49 major disadvantage of unstructured ocean model grids for their application in efficiently coupled  
50 climate models (Randall et al., 2002). In their review of ocean climate modelling, Griffies et al.  
51 (2000) mention two other problems of unstructured grids: the difficulty to represent the correct  
52 geostrophic balance, and unphysical wave scattering due to grid space variation. Griffies et al.  
53 (2000) state that in most ocean climate models structured grids are implemented. Very often,  
54 generalized orthogonal coordinates are used, which means that the pole problem can be avoided  
55 by shifting the grid pole to the centre of a land mass. Structured grids without orthogonal co-  
56 ordinates exist, too: grids with triangular and with hexagonal grid cells. The latter are called  
57 icosahedral–hexagonal on the sphere (where some few pentagonal grid cells have to be included).  
58 Very recently, these grids have been tested by atmosphere modellers (Ringler et al., 2000; Ma-  
59 jewski et al., 2000; Tomita et al., submitted). The results are similar to those obtained with  
60 spherical orthogonal coordinates (often used in atmosphere models), but the theoretical projec-  
61 tion of computation times looks definitely better for icosahedral–hexagonal grids. This is one of  
62 the reasons why Randall et al. (2002) recommend these grids for climate modelling, both for  
63 atmosphere models and for ocean models.

64 In this paper, we investigate how the grid geometry influences the spreading of convection, i.e.  
65 the spatial enlargement of convective regions, in ocean climate models. For this purpose, we use a  
66 simplified two-layer model with a conceptual representation of ocean dynamics and compare the  
67 features of rectangular grids with those of a grid with hexagonal grid cells (i.e. icosahedral–  
68 hexagonal grids on the sphere).

69 Hecht et al. (2000) state in favour of such conceptual experiments that the “evaluation of  
70 schemes may be facilitated through the consideration of simpler [...] test problems, designed to  
71 challenge the performance of algorithms in fundamental, important ways.” In Hecht et al. (2000),  
72 a new test problem for ocean tracer transport is presented. The rotation of the grid by 45° is the  
73 essential test ingredient. The authors find a sensitivity to the orientation of the model grid. In our  
74 paper, we also address the question of horizontal (an)isotropy.

75 The interaction between the convective adjustment scheme and horizontal eddy diffusion has  
76 been studied in a conceptual way by Cessi and Young (1996). They show that there is a strong  
77 sensitivity to initial conditions and that simulation runs with similar initial conditions can lead to  
78 solutions with very different average properties. In Cessi (1996) an instability on the grid scale is  
79 described. The instability is caused by the convective adjustment scheme.

80 The paper is organized as follows: it starts in Section 2 with the description of the two-layer  
81 ocean model used for our investigation. Section 3 is devoted to numerical experiments in which  
82 the spatially averaged effect of grid geometry is examined. This is done by using the atmospheric  
83 boundary condition for heat flux as a hysteresis parameter. The sensitivity to the direction of  
84 advection is studied in Section 4. For this purpose, a homogeneous advective field is added to the  
85 equations. Section 5 contains results with a hexagonal grid for both test experiments (hysteresis  
86 and directional sensitivity). The effect of isopycnal mixing is investigated in Section 6. Conclusions  
87 are given in Section 7.

## 88 2. Description of the model with square grid cells

89 We study the mechanisms of discretization effects that occur when convection spreads in ocean  
90 climate models. By *spreading of convection* we mean the spatial enlargement of an area of con-  
91 vective grid cells. To address general features of the problem, the model we use is strongly sim-  
92 plified. Nevertheless, it captures convective mixing and eddy-diffusion; including advection is an  
93 additional option. Since the local, parameterized convection process and its modification by  
94 horizontal coupling through eddy-diffusion (and advection) is the focus of our interest, we use the  
95 temperature and the salinity as prognostic variables and neglect the momentum budget. The  
96 model possesses two vertical layers, and its horizontal scale is of the same magnitude as the basin  
97 scale. It has a horizontal grid resolution of  $\Delta x = 250$  km and  $16 \times 16$  grid points. We assume that  
98 the volume of the lower grid point is twice the volume of the upper one. This ratio mimics the  
99 increasing layer thickness (with increasing depth) in ocean models. The dynamics at the grid  
100 points is determined by convective mixing (achieved through convective adjustment: CA) and  
101 lateral eddy-diffusive mixing  $D$ . In the upper layer, surface fluxes (freshwater and heat) and op-  
102 tional advection  $A$  (described in Section 4) are added. Omitting the horizontal indices, the  
103 prognostic equations read

$$\frac{\partial}{\partial t} T^{(1)} = \frac{1}{\tau_r} (T_r - T^{(1)}) + D_{T^{(1)}} \quad \{+A_{T^{(1)}}\} \quad [+CA] \quad (1)$$

$$\frac{\partial}{\partial t} S^{(1)} = F_{\text{salt}} + D_{S^{(1)}} \quad \{+A_{S^{(1)}}\} \quad [+CA] \quad (2)$$

$$\frac{\partial}{\partial t} T^{(2)} = D_{T^{(2)}} \quad [+CA] \quad (3)$$

$$\frac{\partial}{\partial t} S^{(2)} = D_{S^{(2)}} \quad [+CA] \quad (4)$$

108  $T^{(1)}$  and  $S^{(1)}$  are the temperature and salinity of an upper grid point at time  $t$ , while  $T^{(2)}$  and  $S^{(2)}$   
 109 represent the respective lower grid point. For the surface fluxes, we use mixed boundary condi-  
 110 tions: a constant freshwater flux  $F_{\text{salt}}$  in combination with the temperature of the upper grid point  
 111 being relaxed towards a restoring temperature  $T_r$ . Mixed boundary conditions are widely used to  
 112 represent the thermally strong coupling between the ocean surface layer and the atmosphere,  
 113 while a similar salinity feedback is absent. For the freshwater flux  $F_{\text{salt}}$ , we use the estimate  
 114  $-1 \times 10^{-4}$  psu d<sup>-1</sup>. Thus, the surface layer is slowly freshened which corresponds to climatic  
 115 conditions at high latitudes (where precipitation exceeds evaporation). The temperature restoring  
 116 timescale  $\tau_r$  is chosen to be five months. This timescale can be derived from observational data, see  
 117 Kuhlbrodt et al. (2001). A Euler forward scheme with a time step  $\Delta t$  of one day is applied. After  
 118 each iteration, a simple *convective adjustment* (CA) scheme is carried out: if the vertical density  
 119 difference  $\rho_1 - \rho_2$  becomes zero or larger, the two grid cells will be mixed completely. Here, a  
 120 linear approximation of the density equation is used

$$\rho(T, S) = \rho_0(1 + \beta(S - S_0) - \alpha(T - T_0)) \quad (5)$$

122 The index 0 denotes reference values (that are irrelevant here, since we only use the density dif-  
 123 ference);  $\alpha$  and  $\beta$  are the expansion coefficients for temperature and salinity. We use the values  
 124  $\alpha = 0.00017$  K<sup>-1</sup> and  $\beta = 0.0008$  psu<sup>-1</sup>. Since the volume of the lower cell is twice the volume of  
 125 the upper one, the final mixed temperature of the two cells reads in its discretized form

$$T_{t+\Delta t}^{\text{mix}} = \frac{T_{t+\Delta t}^{(1)} + 2T_{t+\Delta t}^{(2)}}{3} \quad (6)$$

127 The local grid cells are coupled horizontally through eddy-diffusion (in Section 4, an advective  
 128 field  $A$  is added). Horizontal coordinate indices are  $i$  and  $j$ ; they refer to longitude and latitude,  
 129 respectively. The diffusion term  $D_{T^{(1)}}$  reads

$$\begin{aligned} D_{T^{(1)}} &= \kappa_h \nabla_h^2 T^{(1)} \\ &\approx \frac{\kappa_h}{(\Delta x)^2} (T^{(1)}(i-1, j) + T^{(1)}(i, j-1) + T^{(1)}(i+1, j) + T^{(1)}(i, j+1) - 4T^{(1)}(i, j)) \end{aligned} \quad (7)$$

131 The eddy-diffusion constant  $\kappa_h$  is set to  $3.0 \times 10^3$  m<sup>2</sup> s<sup>-1</sup> which is a typical value for ocean cli-  
 132 mate models of coarse resolution (Braconnot et al., 1997). The parameter values of the model are  
 133 shown in Table 1. *No flux* boundary conditions are applied.

134 Laplacian diffusion is used here which is one of the simplest eddy diffusion schemes. Today  
 135 higher order schemes (like biharmonic diffusion) are applied more and more often in ocean  
 136 models. Therefore, one may ask why they are not taken into account in this study. But concerning  
 137 the efficiency of coupled climate models, higher order schemes have two disadvantages: high CPU  
 138 costs and unphysical long-range coupling. The computation time required for biharmonic diffu-  
 139 sion is increased by the fact that this scheme is not positive-definite and therefore needs a cor-  
 140 rection term. Every eddy diffusion parameterization has the drawback of unphysical long-range

Table 1  
Parameter values of the conceptual two-layer model

Parameter	Denotation	Value
Grid resolution	$\Delta x$	250 km
Time step	$\Delta t$	1 day
Restoring time scale	$\tau_r$	5 months
Salt flux	$F_{\text{salt}}$	$-1 \times 10^{-4}$ psu d <sup>-1</sup>
Eddy diffusion constant	$\kappa_h$	$3 \times 10^3$ m <sup>2</sup> s <sup>-1</sup>

141 coupling, but if only direct neighbours are taken into account, this drawback will be minimized.  
142 Hence we apply the Laplacian diffusion scheme here and discuss whether another grid geometry  
143 (namely hexagonal grid-cells) can reduce the discretization effects.

144 The ocean can be in a state of bistability with respect to convection, which has been shown by  
145 Lenderink and Haarsma (1994) in simple ocean general circulation models and by Kuhlbrodt  
146 et al. (2001) in conceptual box models. By contrast, here we are rather interested in the transient  
147 behaviour during one period of convection. Hence, with our model, we do not perform long  
148 simulations with constant parameters (maximum integration time: 160 days), and we do not  
149 distinguish between two stable states but between two different local *transients*: one that is per-  
150 manently convective (CA at every time step) and another one that is initially non-convective but  
151 may become convective during the simulation. The onset of convection is characterized by a jump  
152 of the values of the variables.

### 153 3. Average behaviour: hysteresis curves with artificial steps

154 The first effect to be studied is the *average* behaviour of an area in the ocean model with  
155 convective and non-convective grid points, when temporarily strong buoyancy forcing prevails at  
156 the surface. Thus, a transition of non-convective elements to convection is favoured. We use two  
157 alternative types of initial conditions (IC) for each pair  $(i, j)$  of horizontal coordinates—convective  
158 IC and non-convective IC

$$T_{\text{con}}^{(1)} = T_{\text{con}}^{(2)} = 4 \text{ }^\circ\text{C} \quad (8)$$

$$S_{\text{con}}^{(1)} = S_{\text{con}}^{(2)} = 35 \text{ psu} \quad (9)$$

$$T_{\text{non}}^{(1)} = 0 \text{ }^\circ\text{C} \quad (10)$$

$$S_{\text{non}}^{(1)} = 33.7 \text{ psu} \quad (11)$$

$$T_{\text{non}}^{(2)} = 4 \text{ }^\circ\text{C} \quad (12)$$

$$S_{\text{non}}^{(2)} = 35 \text{ psu} \quad (13)$$

165 The IC are randomly distributed with the ratio

$$R_0 = \frac{n_{0,\text{con}}}{n_{0,\text{non}} + n_{0,\text{con}}}$$

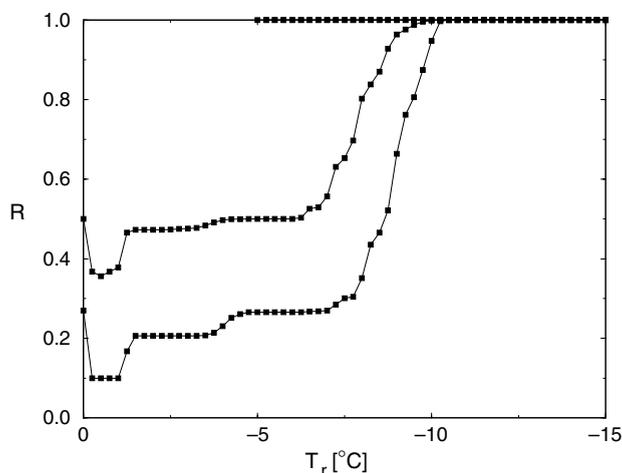


Fig. 1. Hysteresis curves for  $R_0 = 0.5$  (upper curve) and  $R_0 \approx 0.27$  (lower curve). The restoring temperature  $T_r$  is the hysteresis parameter. We average over 200 realizations with randomly distributed initial conditions (but fixed  $R_0$ ).

167 between the number of convective and all grid cells. The hysteresis run consists in a step-  
 168 wise decrease and increase of the surface restoring temperature  $T_r$ . After two time steps,  $T_r$   
 169 changed by  $0.25\text{ }^\circ\text{C}$ . We use a time step of one day. The hysteresis curve starts at  $T_r = 0\text{ }^\circ\text{C}$ ,  
 170 turns at  $T_r = -15\text{ }^\circ\text{C}$ , and ends at  $T_r = -5\text{ }^\circ\text{C}$ . We average over 200 realizations of the hysteresis  
 171 run.

172 In Fig. 1, the ratio  $R$  between convective and all grid cells is shown depending on the restoring  
 173 temperature  $T_r$ . Two hysteresis curves for different initial ratios  $R_0$  are presented: one for  $R_0 = 0.5$   
 174 and one for  $R_0 \approx 0.27$  (68 convective elements). In both cases, the curve jumps to a value  $R < R_0$   
 175 within one step of the hysteresis parameter, because of single convective elements that have only  
 176 non-convective neighbours do not remain convective after the first time step with the initial  $R_0$   
 177 chosen. Convection is suppressed by eddy-diffusive transport from neighbour grid cells. Naturally,  
 178 this effect is larger for  $R_0 \approx 0.27$ , since the probability of convective elements having no convective  
 179 neighbour is larger. The decrease of the restoring temperature does not lead to a continuous  
 180 increase of  $R$ , but the increase occurs stepwise. In both cases ( $R_0 = 0.5$  and  $R_0 \approx 0.27$ ), two steps to  
 181 the left of the steep slope at  $-8\text{ }^\circ\text{C}$  can be distinguished. At lower restoring temperatures (around  
 182  $-8\text{ }^\circ\text{C}$ ),  $R$  quickly approaches the value 1 in both curves of Fig. 1, and  $R = 1$  remains until the  
 183 restoring temperature reaches  $-15\text{ }^\circ\text{C}$  where the direction of restoring temperature change is re-  
 184 versed. The system remains in a totally convective state, while the restoring temperatures are  
 185 increasing again. Hence, the system exhibits hysteretic behaviour. The hysteresis curves end at  
 186  $T_r = -5\text{ }^\circ\text{C}$ , since we do not want to study the transition back to non-convective conditions here.

187 The steps between  $T_r = -0.5\text{ }^\circ\text{C}$  and  $T_r = -2\text{ }^\circ\text{C}$  and between  $T_r = -2\text{ }^\circ\text{C}$  and  $T_r = 5\text{ }^\circ\text{C}$  in-  
 188 dicate that *discretization effects* are at work. They are caused by thresholds of local patterns in the  
 189 model grid. This effect is similar to the one described by Vellinga (1998) who attributed the  
 190 multistability of a model ocean to a CA-related local bistability. The latter gives rise to a finite  
 191 number of thresholds at which single grid points switch between the non-convective and the

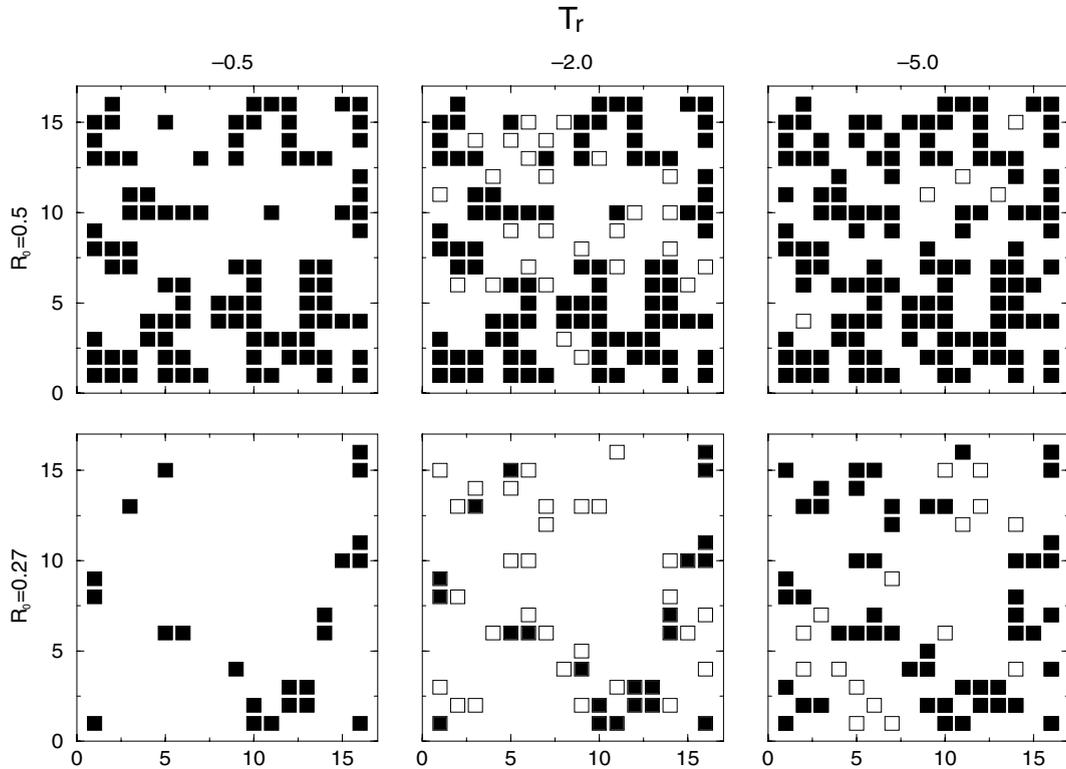


Fig. 2. Thresholds of small patterns determine hysteresis steps. Snapshots of two single realizations during the hysteresis run are shown here. Upper row:  $R_0 = 0.5$  for  $T_r = -0.5$  °C (left),  $T_r = -2$  °C (centre), and  $T_r = -5$  °C (right). Lower row:  $R_0 \approx 0.27$  for  $T_r = -0.5$  °C,  $T_r = -2$  °C, and  $T_r = -5$  °C. Convective grid points are represented as filled squares; new convective grid points (in comparison with the respective figure to the left) as empty squares.

192 convective state. In Fig. 2, the distribution of convective grid points before and after the major  
 193 steps is shown; black squares denote convection. In our case, even for *averaged* hysteresis curves  
 194 with *randomly* distributed IC, the discretization effect is visible: the hysteresis curves exhibit a  
 195 staircase-like behaviour. Thus, it cannot be argued that weather fluctuations of the atmosphere or  
 196 the ocean would cause discretization effects in ocean climate models to disappear (“average them  
 197 out”). By contrast, discretization effects might lead to *systematic errors* on the average.

198 If one takes a closer look at the change of the convective patterns in Fig. 2, one will see that the  
 199 two jumps of the hysteresis curves in Fig. 1 refer to two different transitions

- (1) At  $T_r = -2$  °C, *direct* neighbours of convective cells and some grid point pairs within non-convective areas have become convective. Thus, a threshold for direct neighbours of convective grid points has been overcome. The grid point pairs become convective because they initially (at  $T = 0$  °C) had a convective IC but non-convective neighbours, suppressing convection during the first steps of the hysteresis curve. When  $T_r$  is decreased, switching to convection becomes possible. The same holds for some few switching grid points at the grid boundary. Possibly these three small pattern switches are not fully identical, but together they obviously make up the step in the hysteresis curve.
- (2) At  $T_r = -5$  °C, the new convective grid points correspond to a *checkerboard* pattern that can sometimes be found in ocean climate models. In this pattern, the convective (and non-convective) grid points are distributed like the black (or white) fields on a checkerboard.

211 Based on a statistical analysis, the two patterns responsible for the two steps can be distin-  
212 guished. First, we define the number  $N_{\text{dir}}$  of direct, convective neighbours of a grid cell that has  
213 just become convective. Numerically, it is found for arbitrarily many realizations that

$$N_{\text{dir}}(T_r = -2 \text{ °C}) = 1 \quad N_{\text{dir}}(T_r = -5 \text{ °C}) = 0$$

215 hold for both initial ratios  $R_0$  and every new convective grid cell. The step between  $T_r = -0.5$  °C  
216 and  $T_r = -2$  °C is related to additional convection in grid cells with exactly one convective  
217 neighbour cell. But this result does not yet tell anything about the pattern responsible for the  
218 second step. In order to find out whether a *checkerboard* pattern can be discovered, every grid cell  
219 with the indices  $(i \pm 2, j)$ ,  $(i, j \pm 2)$ , or  $(i \pm 1, j \pm 1)$  is defined as one of the eight checkerboard  
220 neighbours of the grid cell with the indices  $(i, j)$ . The definition is illustrated in Fig. 4.

221 Fig. 3 shows probability distributions of the number  $N_{\text{chess}}$  of convective checkerboard neigh-  
222 bours for the two initial ratios  $R_0$ . In the case  $R_0 = 0.5$ , the majority of newly convecting cells has 4  
223 or more convective checkerboard neighbours. In the case  $R_0 \approx 0.27$  however, about 8% of the new  
224 convective grid cells have no convective checkerboard neighbour. We conclude that the check-  
225 erboard pattern becomes the more important the more convective cells already exist. Boundary  
226 grid cells are excluded from the analysis of the patterns.

227 The mechanism of the described discretization effect can be studied and explained with even  
228 simpler models: in Lind et al. (accepted) and Titz (2002), a lattice of coupled bistable maps was  
229 used in order to study phenomena like the staircase shape of hysteresis curves (and the sensitivity  
230 of advection which we show in the next section). It turned out that such discretization effects can  
231 be described by a local bistability that is represented by one prognostic equation and the re-  
232 spective diffusive coupling operator.

#### 233 4. Sensitivity to the direction of advection

234 Advection plays an important role during the development of a convective area in the ocean.  
235 But in the context of our study it may *hide* certain discretization effects if geostrophic adjustment  
236 is incorporated in the model. Here we investigate whether there might exist a significant sensitivity  
237 to the direction of advection. Therefore a *homogeneous*, unidirectional advective field is added to  
238 our model equations. In other words, the advantage of conceptual clarity is paid for with a less

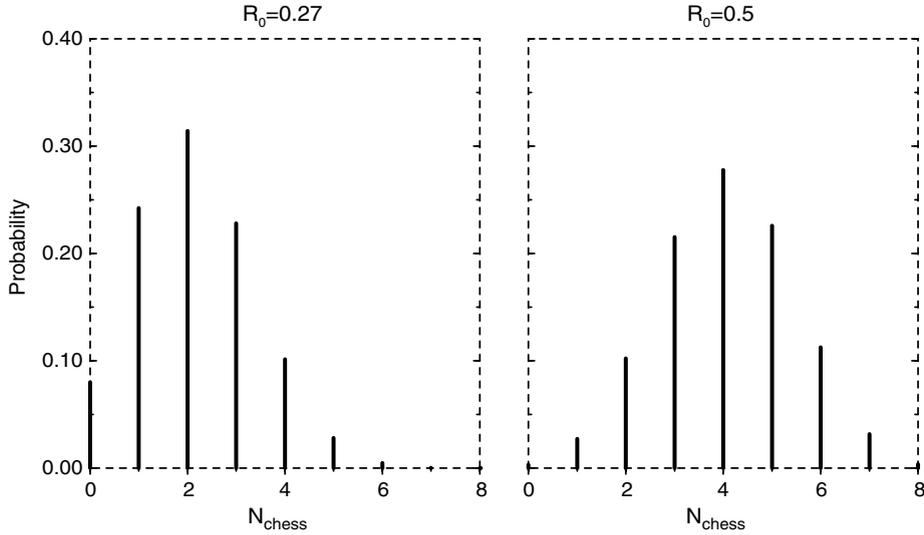


Fig. 3. Probability distributions of the number of convective checkerboard neighbours that a new convective grid cell will have. This figure refers to the step on the hysteresis curve between  $T_r = -2$  °C and  $T_r = -5$  °C. 500 000 realizations are used.

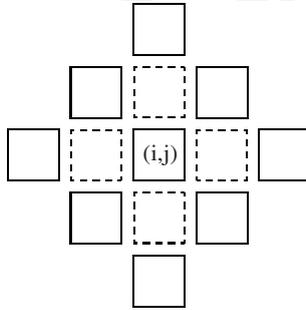


Fig. 4. The checkerboard neighbour cells of the cell  $(i,j)$  are depicted as solid squares.

239 realistic velocity field. The prognostic equations of the surface variables are extended by an ad-  
240 vective term  $A$ . For discretization, the centered differences scheme is used

$$A_{T^{(1)}} = \mathbf{v}_h \cdot \nabla_h T^{(1)} \approx \frac{1}{2}u(T^{(1)}(i-1, j) - T^{(1)}(i+1, j)) + \frac{1}{2}v(T^{(1)}(i, j-1) - T^{(1)}(i, j+1)) \quad (14)$$

242 The horizontal coordinates  $u$  and  $v$  of the velocity vector correspond to the polar coordinates  $\theta$   
243 and  $|\mathbf{v}|$ , the angle and the amplitude of the advective velocity vector

$$u = |\mathbf{v}| \cos \theta$$

$$v = |\mathbf{v}| \sin \theta$$

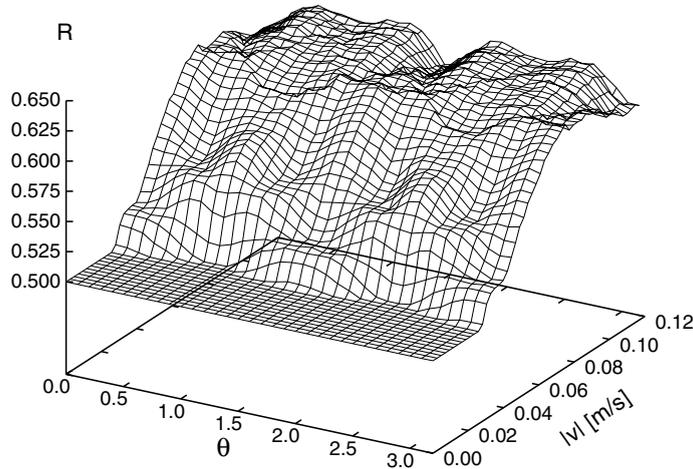


Fig. 5. Sensitivity to the direction of advection. The atmospheric restoring temperature  $T_r$  is set to be  $-5^\circ\text{C}$ .  $\theta$  is the angle of the advective velocity and  $|v|$  its amplitude.  $R$  is the average value of 200 realizations with randomly distributed  $T_s$ .

246 As in the hysteresis experiments, we use *no flux* boundary conditions for the diffusion. The  
247 boundary condition for the advection term of a boundary element ( $i = 1, 2 \leq j \leq 15$ ) reads

$$A_{T^{(1)},\text{boundary}} \approx \frac{1}{2}u(\underline{T^{(1)}(i,j)} - T^{(1)}(i+1,j)) + \frac{1}{2}v(T^{(1)}(i,j-1) - T^{(1)}(i,j+1)) \quad (15)$$

249 Thus, the quantity advected from the boundary (underlined) is set to be identical to the element  
250  $(i,j)$ , so that the boundaries do not influence the dynamics via advection.

251 For a ratio  $R_0 = 0.5$  and a realistic range of the angle and the amplitude of the advective ve-  
252 locity, the ratio  $R$  after 40 days is simulated. 200 realizations of the experiment are done. The  
253 average result is shown in Fig. 5. When  $|v|$  has crossed a threshold, the convective area may  
254 become larger. The final ratio  $R$  does not only depend on the amplitude of the advective velocity  
255 but also on its angle  $\theta$ . This double dependence is obvious in Fig. 6 that displays the contour lines  
256 of  $R$ . Differences in the final value of  $R$  for the same  $|v|$  can amount to up to 10%. Previously, this  
257 kind of horizontal anisotropy was found e.g. by Hecht et al. (2000) who studied advection  
258 schemes with rotated grid orientation. They found that a standard wind-driven gyre as a test case  
259 is simulated differently with the grid tilted by  $45^\circ\text{C}$ . In addition, our results indicate that local  
260 bistability increases the anisotropic effect strongly.

## 261 5. Hexagonal grid cells versus square grid cells

262 Model grids with hexagonal grid cells (Fig. 7) have been used for the first time by atmosphere  
263 modellers (Sadourny et al., 1968; Williamson, 1968). The sphere can be covered with hexagons  
264 and a few pentagons in a very homogeneous way (Baumgardner and Frederickson, 1985; Tomita  
265 et al., 2002), avoiding the pole problem, while in the plane, hexagons can be used exclusively.  
266 Together with triangles and squares, hexagons are the only regular polygons that can tile a plane,

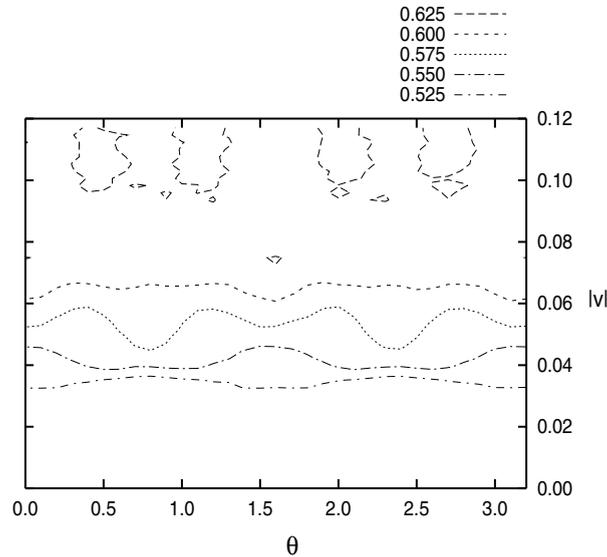


Fig. 6. Contour plot of the sensitive dependence of  $R$  on  $\theta$  and  $|v|$  in Fig. 5. The angle  $\theta$  for which  $R$  has a maximum is not fixed but depends itself on  $|v|$ .

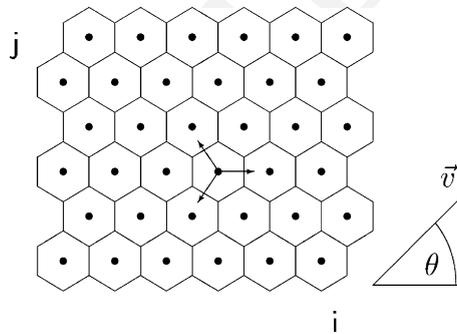


Fig. 7. Sketch of a grid with hexagonal grid cells. Each grid cell has six neighbour cells. On the right hand side, the velocity vector  $\vec{v}$  and the corresponding advection angle  $\theta$  are shown. They are used in the advection experiments of Section 5.2.

267 and hexagons have the highest symmetry of the three polygons. This guarantees a good horizontal  
 268 isotropy, which manifests itself in good test results concerning wave propagation. Equivalents to  
 269 the common staggered difference grids (Arakawa grids) exist on hexagonal grids; see for example  
 270 Popović et al. (1996). Icosahedral grids have been tested with the shallow-water equations (Heikes  
 271 and Randall, 1995a,b; Thuburn, 1997; Tomita et al., 2001; Ringler and Randall, 2002) and with  
 272 the atmospheric general circulation (Ringler et al., 2000; Majewski et al., 2000; Tomita et al.,  
 273 submitted). The propagation of quasi-geostrophic modes was studied analytically on several  
 274 difference grids (Popović et al., 1996). Ničković et al. (2002) investigated the geostrophic ad-

275 justment process on selected hexagonal grids with a simple two-dimensional linearized model of  
276 the atmosphere.

277 In this section of the paper, we show that the good horizontal isotropy and the larger number  
278 of direct local neighbour grid cells (six instead of four) can improve the model behaviour. Es-  
279 pecially for coupled ocean-atmosphere climate models, hexagonal grid cells may be a useful al-  
280 ternative to square grids. Randall et al. (2002) propose that a icosahedral–hexagonal grid could be  
281 used for both the ocean model and the atmosphere model, and in coastal areas, hexagonal grids  
282 could be additionally refined, in a similar way as rectangular grids.

283 In the following, the previous experiments are repeated on the hexagonal grid and compared  
284 with those on the square grid. The same distance between neighbouring grid points is used, so that  
285 the area covered by the hexagonal grid is 13% smaller.

### 286 5.1. Hysteresis curves with hexagonal grid cells

287 The hysteresis experiments are repeated on the hexagonal grid. Again, *no flux* lateral boundary  
288 conditions are used. The discretized eddy-diffusion term is adapted to the grid geometry

$$\begin{aligned}
 D_{T^{(1)}} &= \kappa_h \nabla_h^2 T^{(1)} \\
 &\approx \frac{2\kappa_h}{3(\Delta x)^2} (T^{(1)}(i-1, j) + T^{(1)}(i, j-1) + T^{(1)}(i+1, j) + T^{(1)}(i, j+1) \\
 &\quad + T^{(1)}(i\pm 1, j-1) + T^{(1)}(i\pm 1, j+1) - 6T^{(1)}(i, j)) \quad (16)
 \end{aligned}$$

290 The sign of the fifth and sixth right-hand side term alternates depending on  $j$  (see Fig. 7).

291 In Fig. 8, the hysteresis curves for the hexagonal grid are compared with the previous result  
292 (Fig. 1). The two curves look almost the same, except for small  $T_r$ -values. We have already  
293 mentioned that the difference between  $R_0$  and  $R$  at the starting point of the hysteresis curves is  
294 caused by “disappearing” isolated convective elements. In the hexagonal grid, some of those el-  
295 ements “survive”. Since every grid cell has six neighbours instead of four, there are more possi-  
296 bilities how convective and non-convective grid cells are arranged in patterns. The probability of  
297 having a convective neighbour cell is larger, increasing the number of “surviving” convective cells.  
298 In contrast to the square grid, there is no step at  $T_r = -2$  °C.

299 Since the hysteresis curve performed with the hexagonal grid exhibits smaller steps, this grid  
300 seems to behave in a smoother way with respect to the spreading of convective cells.

### 301 5.2. Less anisotropy with hexagonal grid cells

302 Now the sensitivity to the direction of the advective velocity is examined. For the implemen-  
303 tation of advection on the hexagonal grid, a discretized advection term is necessary. Three instead  
304 of two horizontal velocity vector components are used now (see Fig. 7). The velocity components  
305 are expressed by means of the square grid’s velocity amplitude  $|\mathbf{v}|$

$$v_{0^\circ} = \sqrt{\frac{2}{3}} |\mathbf{v}| \cos \theta \quad (17)$$

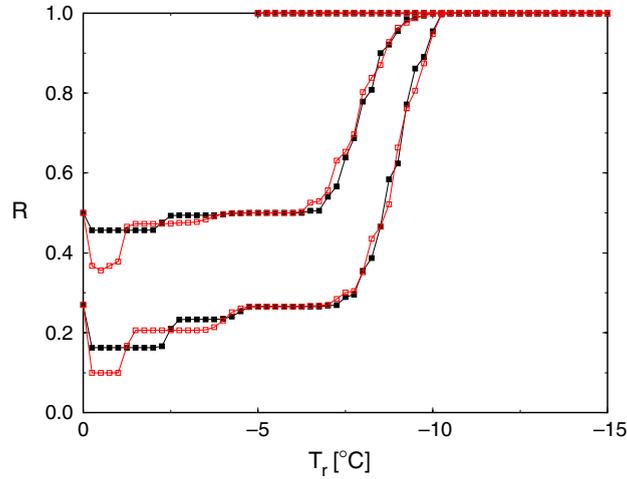


Fig. 8. Hysteresis curves for  $R_0 = 0.5$  (upper curves) and  $R_0 \approx 0.27$  (lower curves). (Filled squares) Hexagonal grid and (empty squares) square grid.

$$v_{120^\circ} = \sqrt{\frac{2}{3}}|\mathbf{v}|\cos(\theta + 120^\circ) \quad (18)$$

$$v_{240^\circ} = \sqrt{\frac{2}{3}}|\mathbf{v}|\sin(\theta - 30^\circ) \quad (19)$$

309 Thus, the advective term for the surface temperature  $T^{(1)}$  reads

$$A_{T^{(1)}} = \frac{1}{2}v_{0^\circ}(T^{(1)}(i, j, \text{up}, 0^\circ) - T^{(1)}(i, j, \text{down}, 0^\circ)) + \frac{1}{2}v_{120^\circ}(T^{(1)}(i, j, \text{up}, 120^\circ) - T^{(1)}(i, j, \text{down}, 120^\circ)) + \frac{1}{2}v_{240^\circ}(T^{(1)}(i, j, \text{up}, 240^\circ) - T^{(1)}(i, j, \text{down}, 240^\circ)) \quad (20)$$

311 where the indices “up” and “down” refer to the upstream and downstream values of temperature  
312 in the grid (see Fig. 7).

313 When the experiment with advection is repeated on the hexagonal grid, less sensitivity to the  
314 direction of the advective velocity is found (see Fig. 9). Nevertheless, the general behaviour re-  
315 mains the same. The different symmetry properties of the hexagonal grid are clearly visible (three  
316 maxima instead of two).

317 The hexagonal grid is preferable because its horizontal isotropy is clearly better than the be-  
318 haviour of the square grid. A similar effect would be caused by taking into account more  
319 neighbour grid cells on the square grid, but this is computationally much more expensive. Note  
320 that the hexagonal grid has more grid points per unit area (for the same horizontal distance  
321 between neighbouring grid points) and that the isotropy-reducing effect still works with a lower  
322 resolution and a computation time that is equivalent to the square grid.

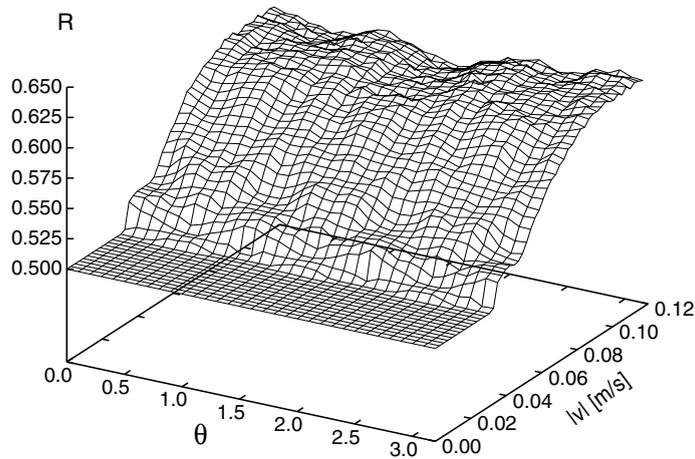


Fig. 9. Less sensitivity to the direction of advection on the hexagonal grid.  $\theta$  is the angle of the advective velocity and  $|v|$  its amplitude. Compare this figure with Fig. 5.

### 323 6. The effect of isopycnal mixing

324 During the last years, purely horizontal tracer mixing has been replaced more and more by  
 325 schemes like the GM scheme (Gent and McWilliams, 1990) that take isopycnal mixing into  
 326 consideration. It turned out that isopycnal mixing may be a useful (although not fully convincing)  
 327 alternative with regard to the occurrence of deep convection events. Therefore, we repeat our  
 328 hysteresis experiments (without advection, see Section 3) with a simplified isopycnal mixing  
 329 scheme: if CA has taken place at a certain grid point, the subsequent eddy-diffusion of the *surface*  
 330 layer at this grid point is performed with the surrounding grid points in the *lower* layer that always  
 331 have approximately the same density as surface grid points after convective mixing. There are no  
 332 other diffusive fluxes. This is no exact isopycnal mixing scheme, but it serves as an approximation  
 333 here. For an upper layer grid cell of the square grid where CA has just occurred, the discretized  
 334 diffusion scheme reads

$$D_{T^{(1)}} \approx \frac{\kappa_h}{(\Delta x)^2} (T^{(2)}(i-1, j) + T^{(2)}(i, j-1) + T^{(2)}(i+1, j) + T^{(2)}(i, j+1) - 4T^{(1)}(i, j)) \quad (21)$$

336 In the grid with hexagonal grid cells, the scheme is computed correspondingly. The diffusion  
 337 scheme for the lower layer grid point is left unchanged.

338 The results in Fig. 10 for both the square grid and the grid with hexagonal grid cells show that  
 339 isopycnal mixing improves the hysteresis curve substantially in our model. There are no such big  
 340 steps in the curve like in Fig. 1. Only on the steep slope of the curve, some few steps are left (see  
 341 zoom in Fig. 11), and again, the hexagonal grid exhibits a smoother behaviour.

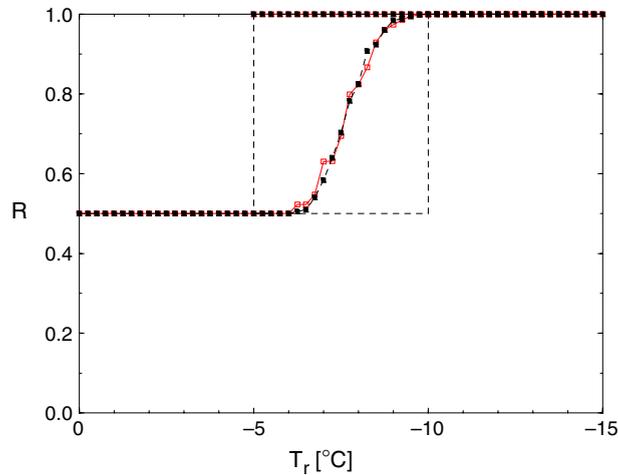


Fig. 10. Hysteresis curves for  $R_0 = 0.5$  with the simplified isopycnal mixing scheme. There are only few small steps left. The hexagonal grid (filled squares) performs better than the square grid (empty squares). The zoom is shown in Fig. 11.

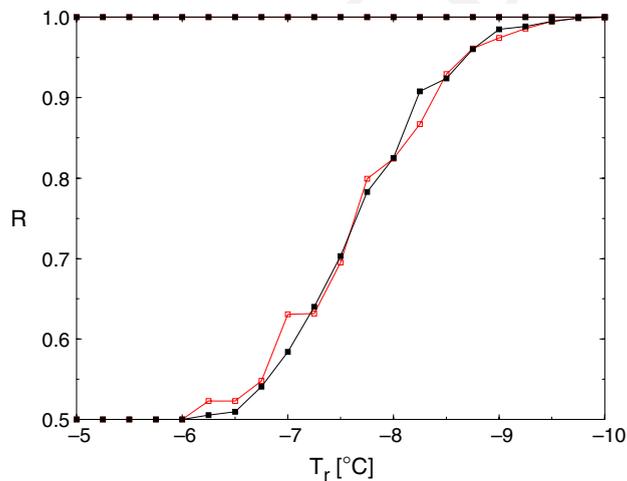


Fig. 11. Hysteresis curves for  $R_0 = 0.5$  with the simplified isopycnal mixing scheme. Zoom from Fig. 10. Filled squares represent the hexagonal grid result and empty squares the square grid result.

## 342 7. Conclusions

343 Strongly non-linear, local processes challenge climate modellers in many ways. There is no  
344 simple, straight path to avoid the problems that these processes cause in climate models—  
345 problems like the difficulties with many parameterizations. One of such local, parameterized  
346 processes is ocean convection. Apart from the question which parameterization scheme is optimal,  
347 it is not irrelevant for the representation of the dynamics which model grid is chosen. In our study

348 that is based on a conceptual two-layer model, we compare the spreading of convection in a  
349 square grid with results obtained using a hexagonal grid.

350 It turns out that the *local* discretization effect manifests itself in the *average* behaviour of an  
351 entire ocean region. This effect is studied in hysteresis experiments in which the surface boundary  
352 condition for heat flux is employed as a hysteresis parameter, and the initial convective activity is  
353 randomly distributed. The discretization effects are visible as steps in an averaged hysteresis curve.  
354 Cessi and Young (1996) have shown the strong sensitivity of the convective adjustment scheme to  
355 initial conditions. In this paper, we demonstrate how small scale pattern switches are associated  
356 with steps in the hysteresis curve. The first of two major steps is related to direct neighbour cells of  
357 convective cells becoming convective, while the second step corresponds to a kind of checkerboard  
358 pattern.

359 Convection in a grid with square grid cells is quite sensitive to the direction of advection. This is  
360 an anisotropy which might yield substantial systematic errors in ocean climate models. The errors  
361 could be hidden due to the more complex velocity patterns in less idealized velocity fields. The  
362 anisotropy is shown here in numerical experiments in which different values for the horizontal  
363 angle of a homogeneous velocity field cause clearly different developments of convective activity.  
364 Hecht et al. (2000) found a similar result for a test experiment with a horizontal ocean gyre and  
365 rotated grids. In their study, it turned out that the representation of the western boundary current  
366 depends strongly on a proper and step-free representation of the coastline. Here, the effect of the  
367 grid anisotropy is rather surprising, since the lateral boundaries do not affect the results.

368 A model grid with *hexagonal* instead of square grid cells reduces the height of the steps in the  
369 hysteresis curves and significantly improves horizontal isotropy. Even for the—already im-  
370 proved—case with mixing of isopycnal type, the difference between the two grid geometries is  
371 recognisable. Such a mixing scheme reduces the discretization effect seen in the hysteresis ex-  
372 periments.

373 From the restricted viewpoint of these conceptual, numerical experiments, we recommend the  
374 hexagonal grid geometry (i.e. icosahedral–hexagonal on the sphere) for ocean climate modelling.  
375 For ocean models alone, unstructured grids may be the more useful alternative, since they allow  
376 for a better representation of complex orographies. In climate models however, hexagonal grids  
377 have another advantage: the flux coupler (between atmosphere and ocean or land surface) in  
378 GCMs can be programmed much more efficiently if the icosahedral–hexagonal grid is used in all  
379 modules of the model (Randall et al., 2002). If higher resolution was locally needed, this could be  
380 done within the framework of hexagonal grid cells (L. Bonaventura, personal communication).  
381 Therefore we strongly suggest to perform test experiments with comprehensive ocean models  
382 using a icosahedral grid in order to assess the potential value of this grid for ocean climate  
383 modelling.

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